

FEEDHORN ANALYSIS FOR PARABOLIC DISH G/T

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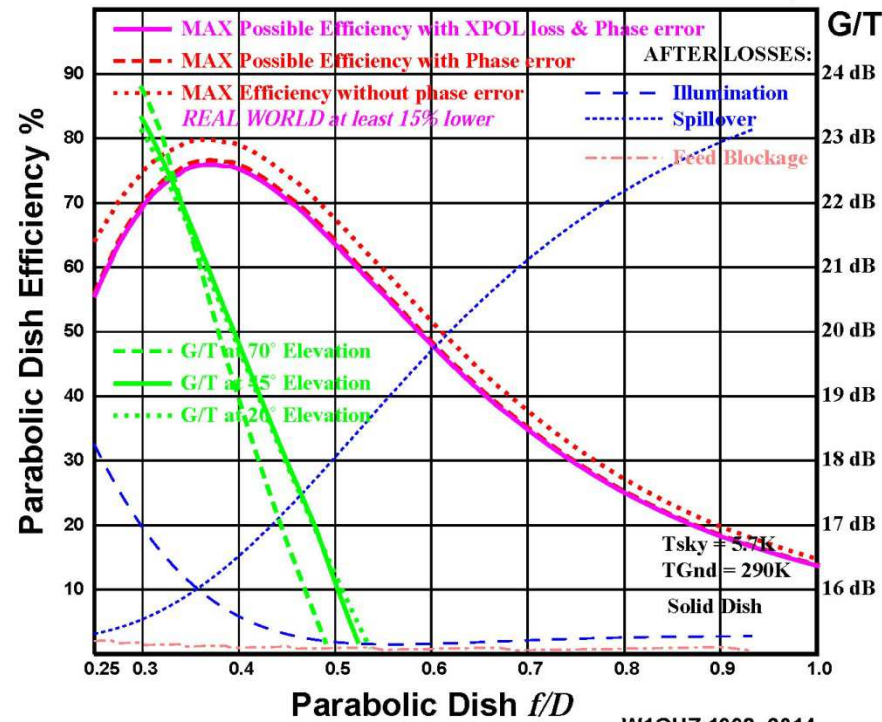
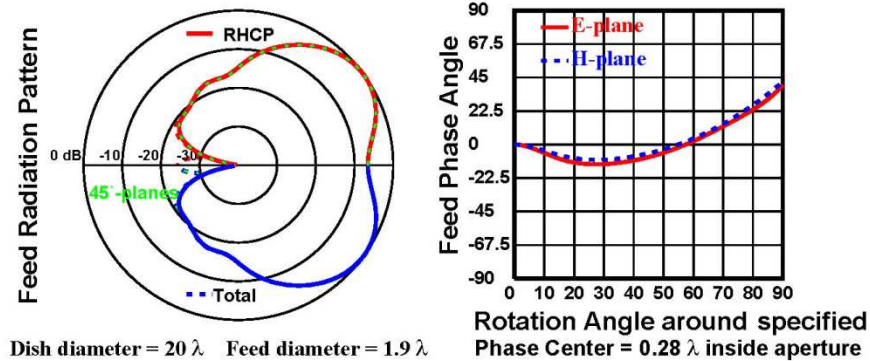
Parabolic Dish Feedhorn Analysis

- Traditionally for efficiency – maximum gain
 - OK for Terrestrial
- G/T calculations
 - OE9PMJ – 1984
 - OE5JFL – 1992
 - OM6AA – 2009, 2011
 - RA3AQ – 2013
 - ONLY for a few feeds and f/D
- Need rapid calculation to compare feedhorns
 - Feed_GT program

Add G/T to Efficiency Plot

Super VE4MA, choke 0.6λ wide x 0.45λ deep, back 0.15λ , RHCP

Figure 1



G/T

- $\frac{G}{T} = \frac{\text{Antenna Gain}}{\text{Noise Temperature (K)}} \rightarrow \frac{\text{Signal}}{\text{Noise}}$

- **Antenna**

- $\frac{G}{T} = \frac{\text{Antenna Gain}}{\text{Antenna Temperature}}$

- **System**

- $\frac{G}{T} = \frac{\text{Antenna Gain}}{\text{Antenna Temperature} + \text{Receiver Noise Temperature}}$

Calculations

- Dish Efficiency

$$\eta = \frac{\iint_{\text{reflector}} U_{CP}(\theta, \phi) \sin\theta d\theta d\phi}{\iint_{\text{all pol}} U_{all}(\theta, \phi) \sin\theta d\theta d\phi} = \frac{\text{Desired polarization on reflector}}{\text{all polarizations } 360^\circ}$$

- Gain

$$G = \eta \frac{4\pi}{\lambda^2} \text{Area} = \text{Efficiency} * \text{Aperture Gain}$$

- Temperature

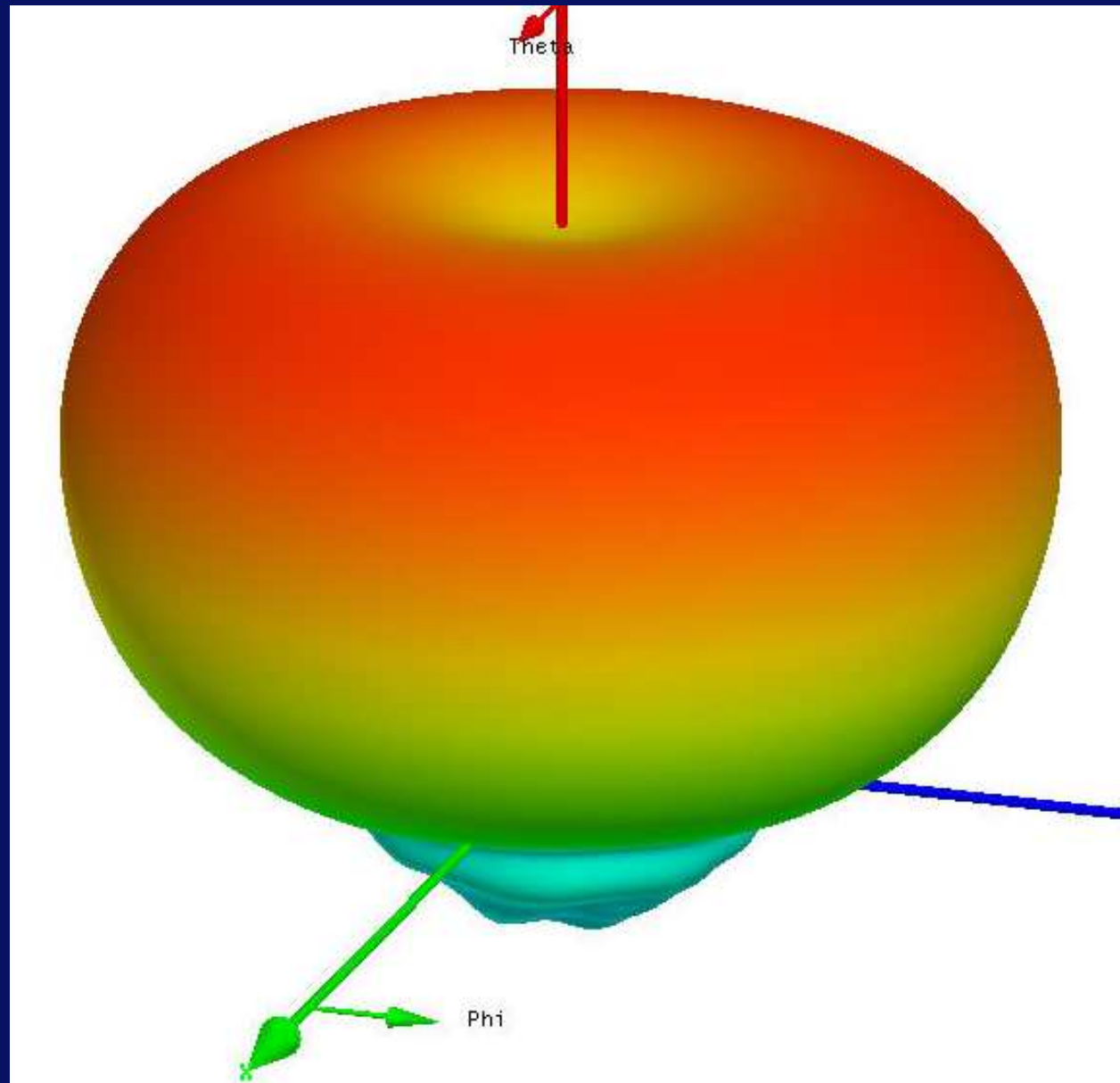
$$T = \iint_{\text{all pol}} \text{Noise}(\theta, \phi) U_{all}(\theta, \phi) \sin\theta d\theta d\phi$$

- $\frac{G}{T} \rightarrow \text{in dB, } 10\log\left(\frac{G}{T}\right)$

Approximations

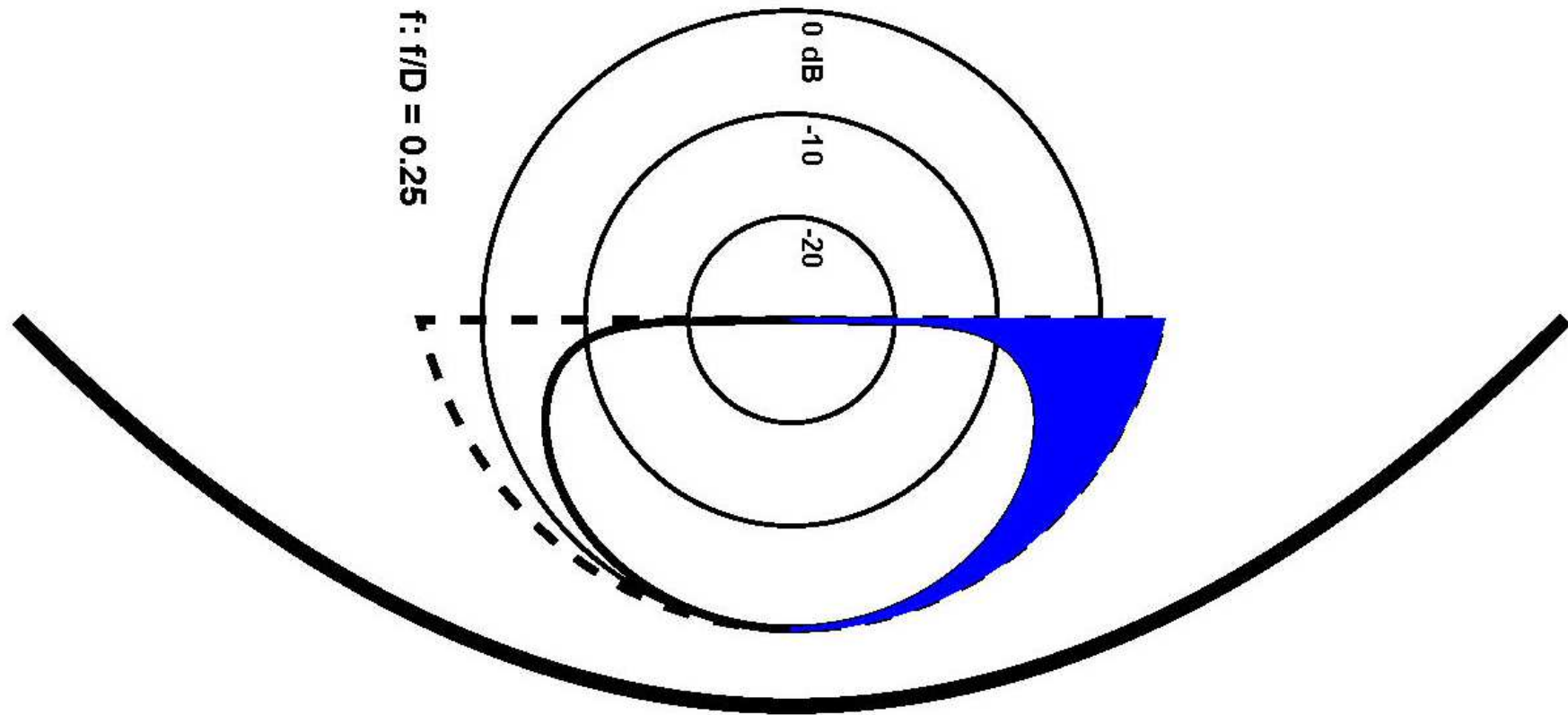
- Well behaved CP feeds
 - Only 0, 45, and 90 degree pattern cuts needed
- No edge diffraction calculation
 - Noise calculation optimistic for very deep dishes
- Sky noise is uniform
 - OK at higher elevation angles
- No interaction between feed and reflector
 - Small effect for large dishes

Well-behaved CP feed pattern



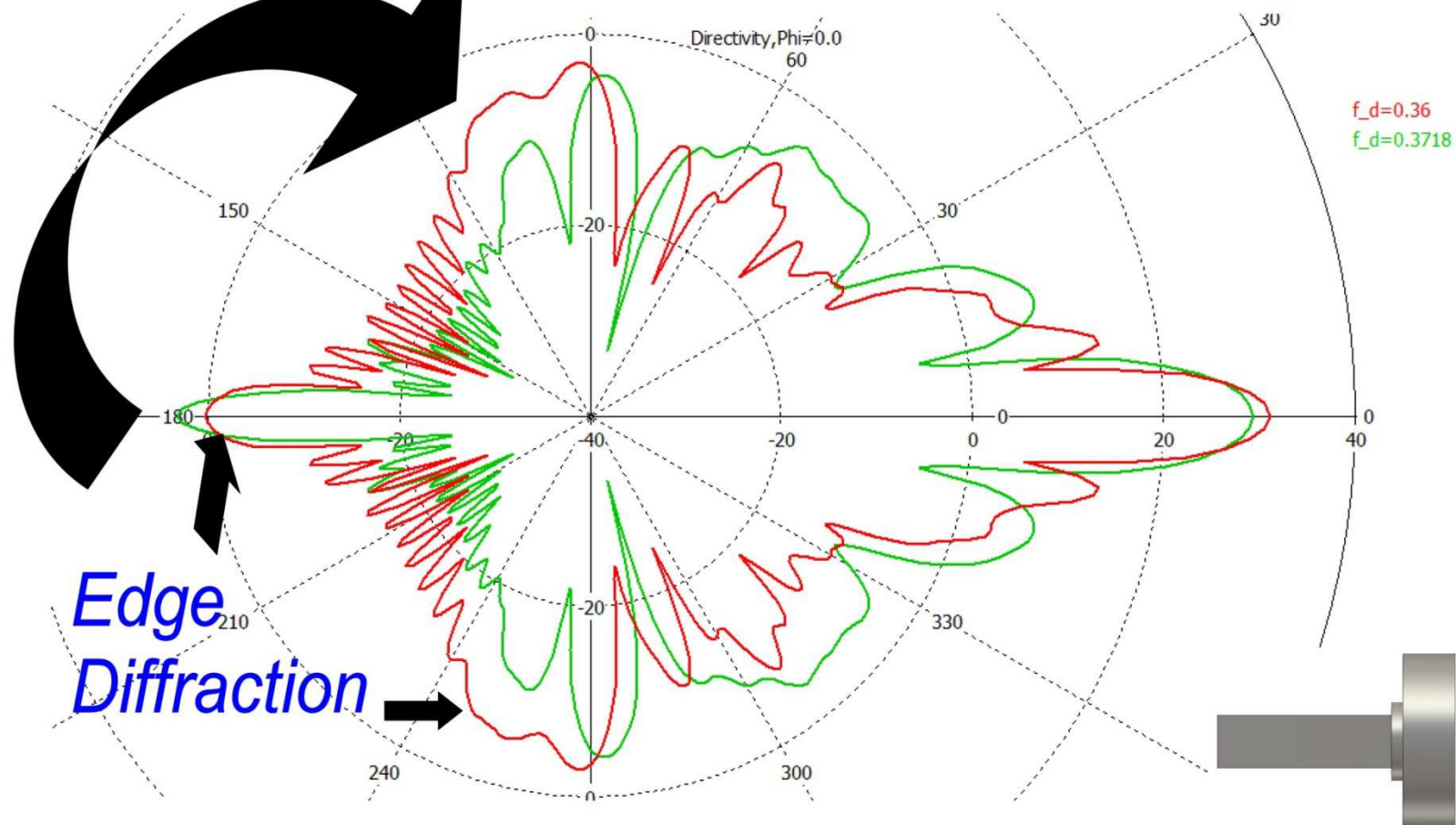
Edge Diffraction - Deep Dishes

Reflector shields feed from ground noise



Edge Diffraction

3m dish with RA3AQ feed
Farfield pattern



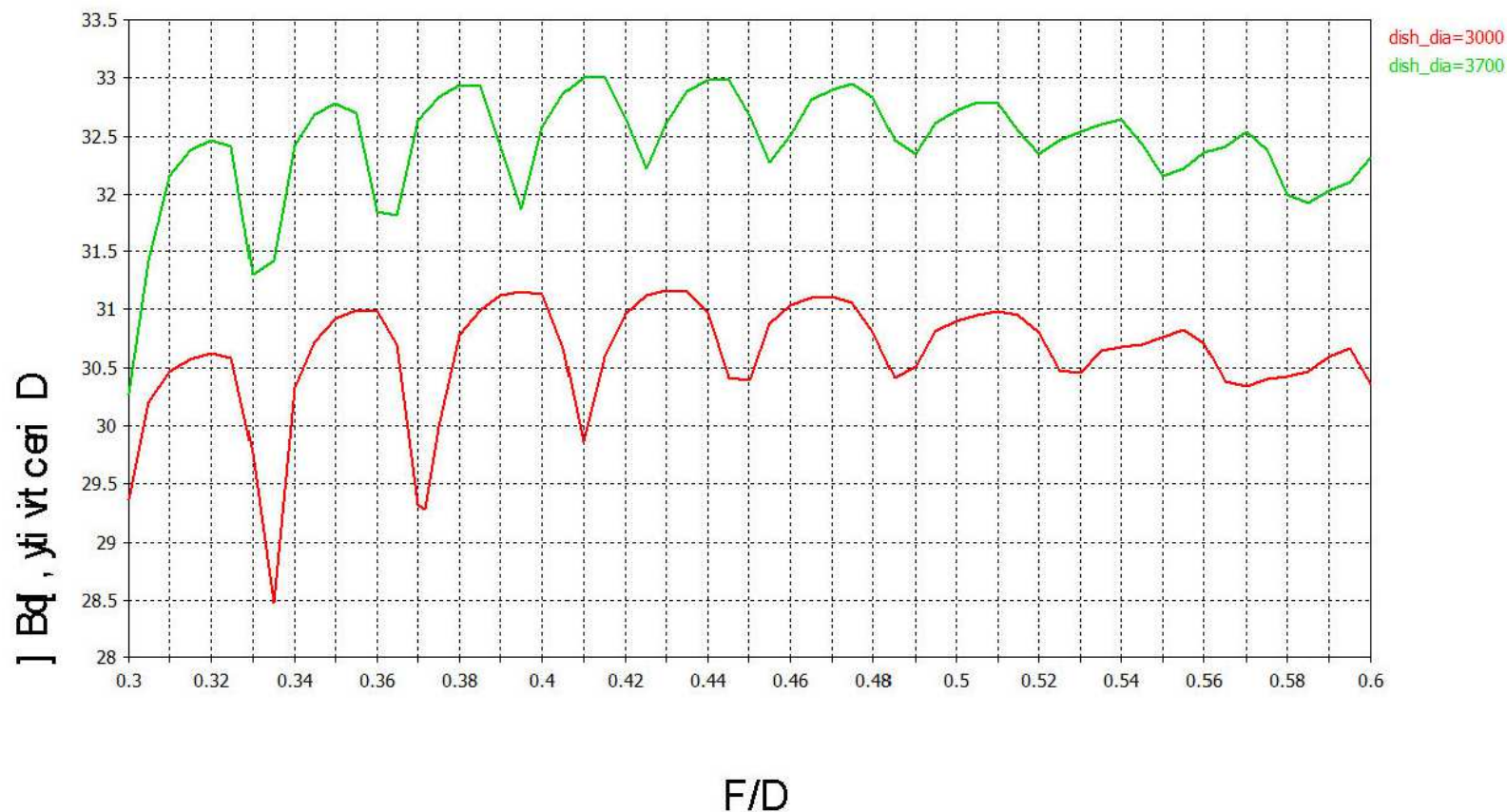
Edge Diffraction

- Edge Diffraction Lobes at 90 and 180 degrees
 - Added ground noise
- Extremely difficult to calculate
- Very deep dishes shield feed from ground
 - Optimistic G/T without Edge Diffraction
- G/T not plotted for $f/D < 0.3$

Interaction between feed and reflector (Mirror Reaction – RA3AQ)

Directivity vs FD for 3m and 3.7m dish

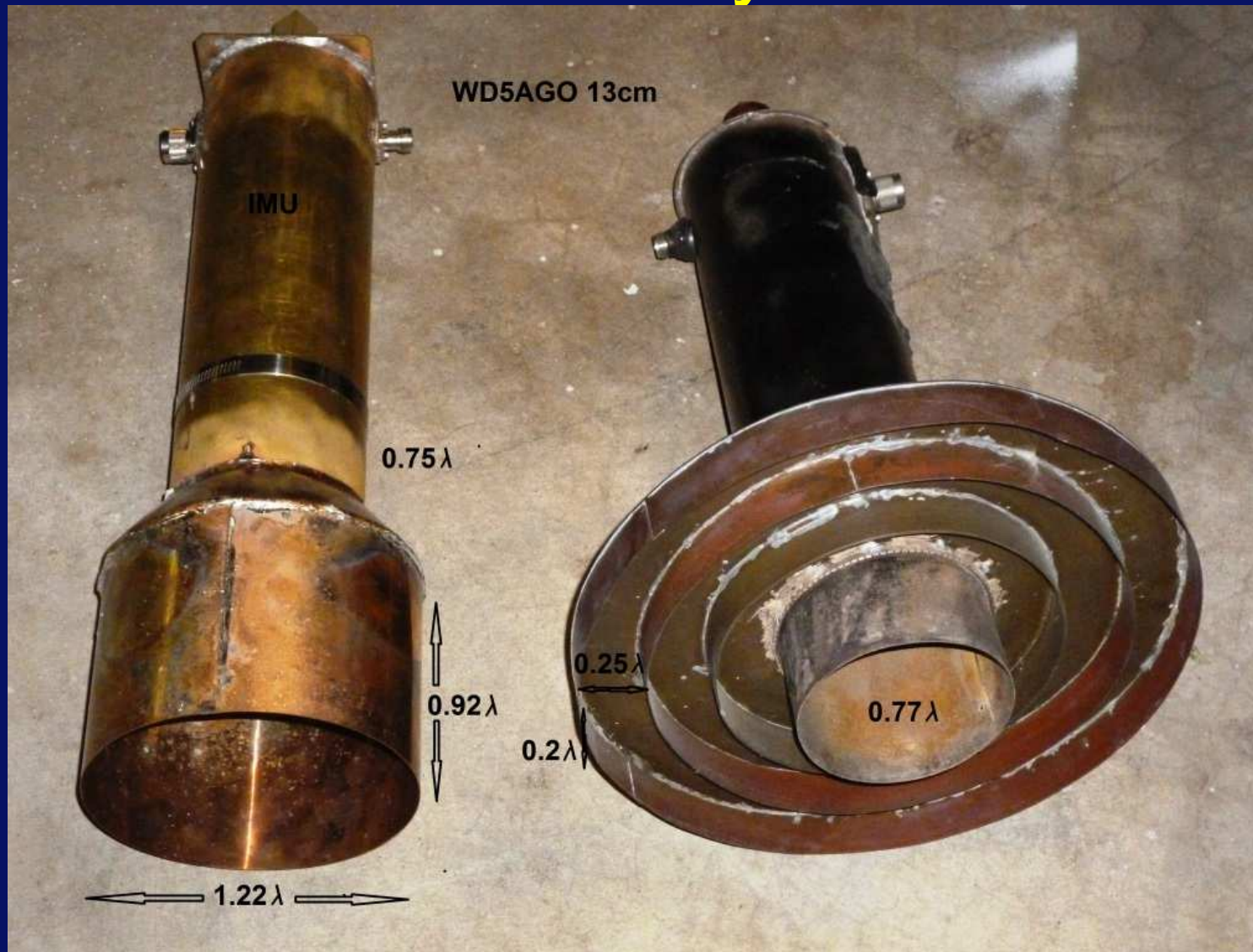
Interaction less for big dishes



Interaction between feed and reflector (Mirror Reaction)

- Interaction is power reflected from dish back into feed
- $\Gamma_m = \frac{G_0 \lambda}{4\pi f}$
- Reflected power mismatch interacts with system Γ
- $\frac{\Delta T}{T} = 4\Gamma_m \Gamma$
- Noise increase
- Mismatches can be tuned to cancel
- **BUT** – CP reverses polarization when reflected
 - Signal goes to other port
 - Noise is not polarized – reflected back

Measurements by WD5AGO



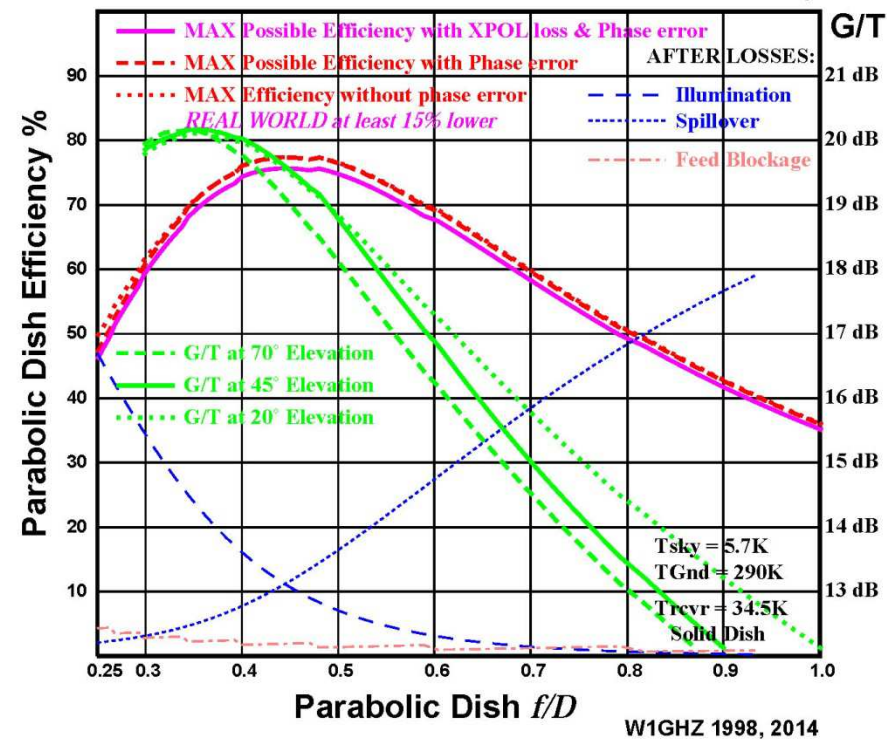
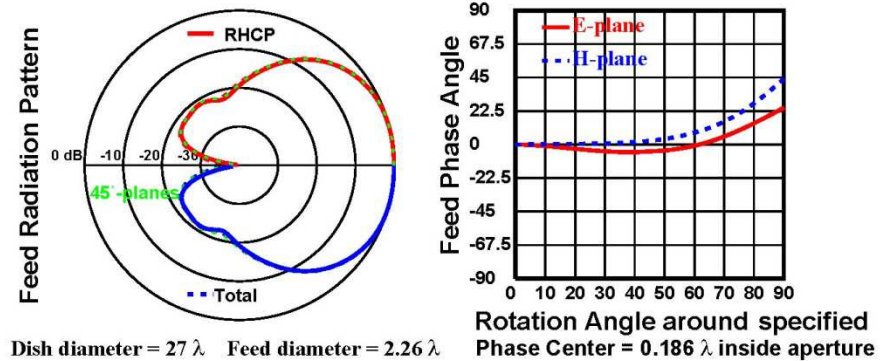
W2IMU

Chaparral

Chaparral 3 rings

Chaparral 3 rings 0.25λ wide x 0.20λ deep, back 0.25λ

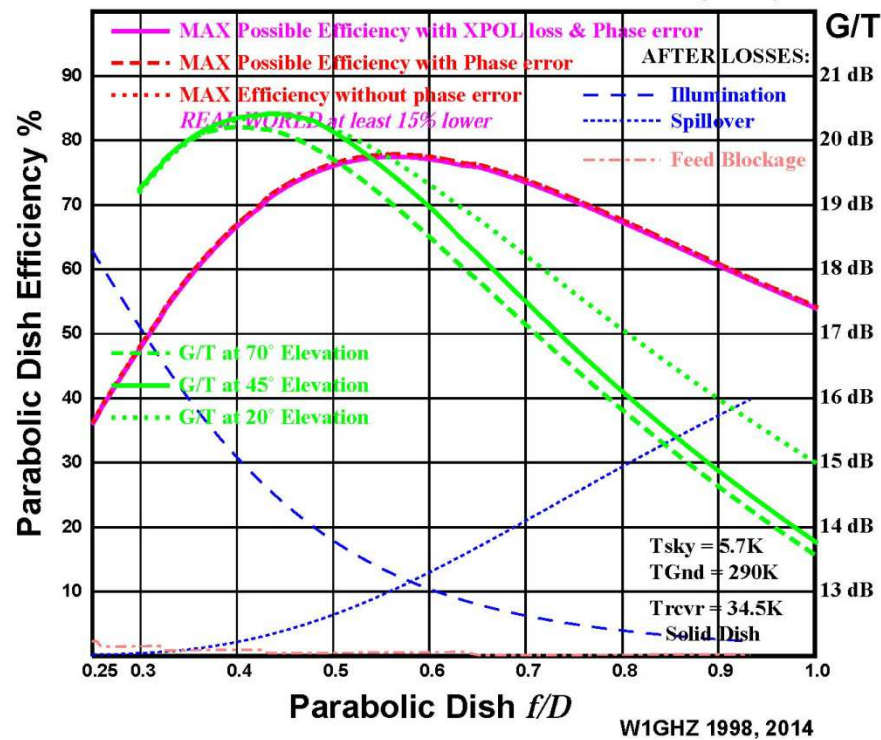
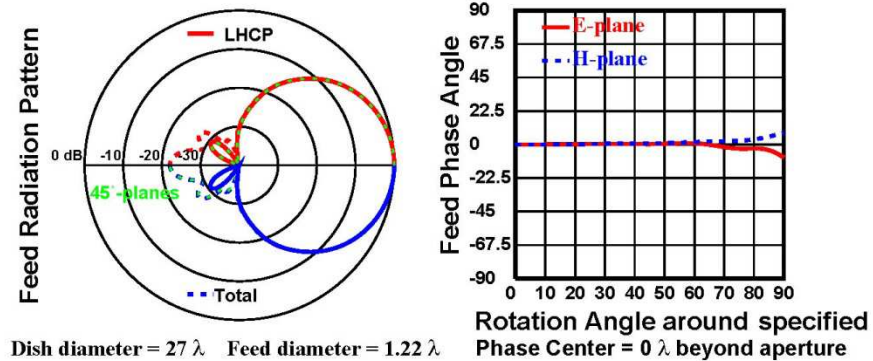
Figure 5



W2IMU 1.22 λ

W2IMU Dual-mode feed 1.22 λ diameter by WD5AGO

Figure 6



Measurements by WD5AGO

27λ dish at 13 cm

Chaparral – 3 ring

- Sun – 16 dB
- Moon – 0.4 dB
- Cygnus A – 0.12 dB

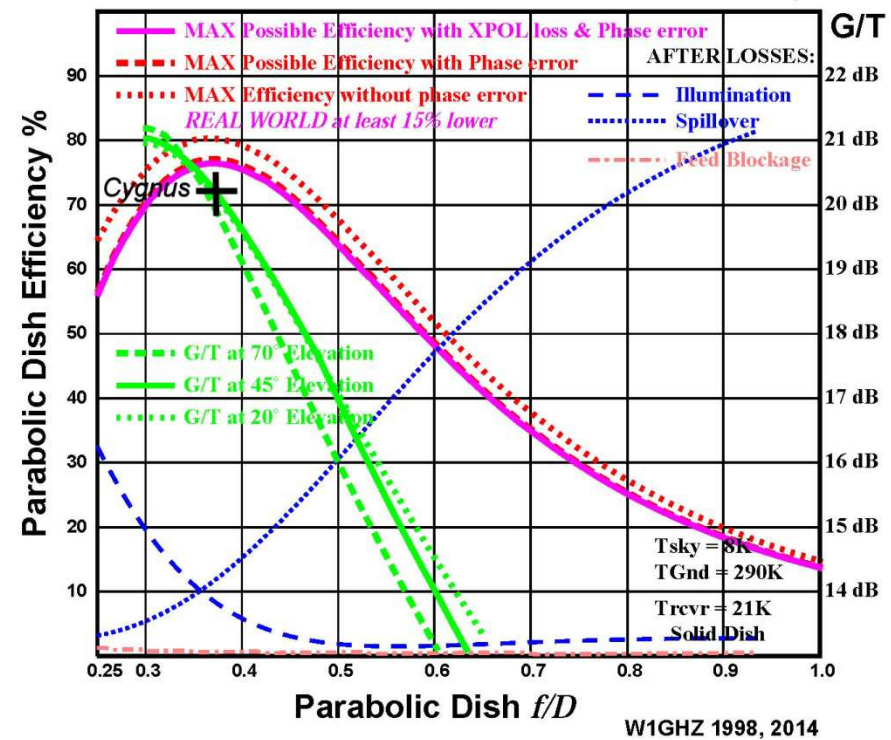
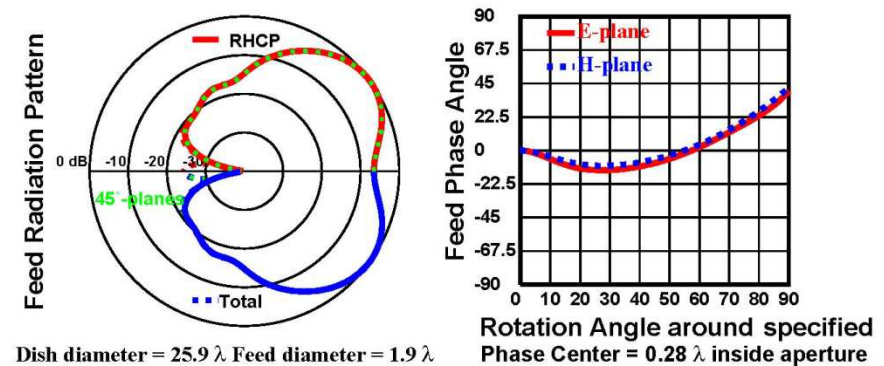
W2IMU – 1.22λ

- Sun – 15.6 dB
- Moon – 0.35 dB
- Cygnus A – 0.10 dB

G3LTF Cygnus A Measurement

$Y = 0.94 \text{ dB}$

G3LTF 23cm SuperVE4MA feed



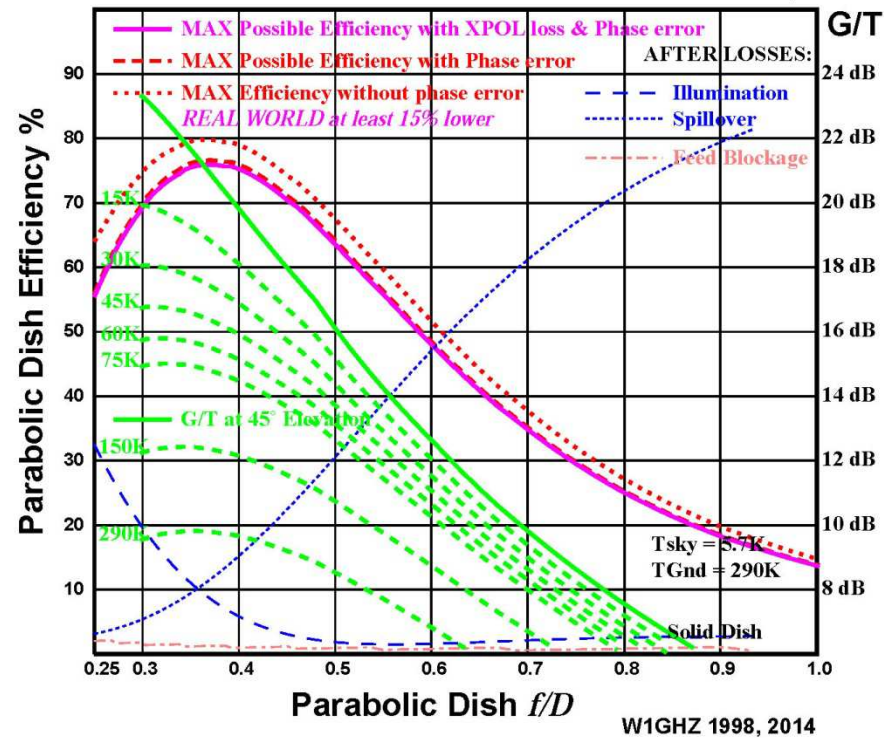
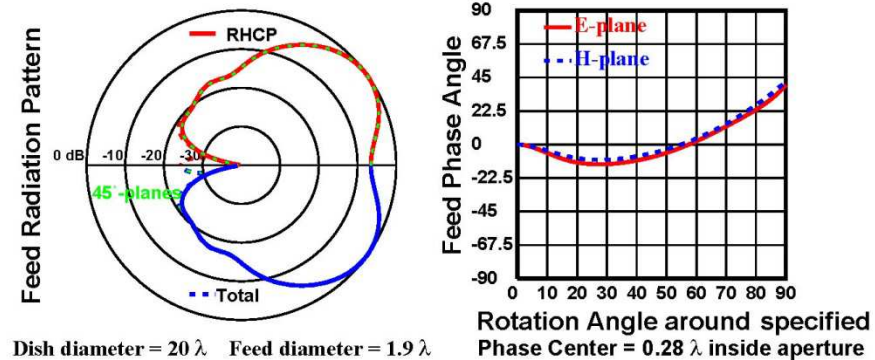
Little Difference between Feeds

- Good feeds have low sidelobes, thus low noise
- Difference is efficiency at various f/D
- Gain proportional to efficiency
 - 60% to 75% = 1 dB
 - 50% to 60% = 0.8 dB
- *Only* a few dB
- Bad feeds have lower efficiency, higher sidelobes

Effect of Receiver Noise Temperature

Super VE4MA, choke 0.6λ wide x 0.45λ deep, back 0.15λ
Receiver Noise Temp Comparison - 15,30,45,60,75,150 & 290K

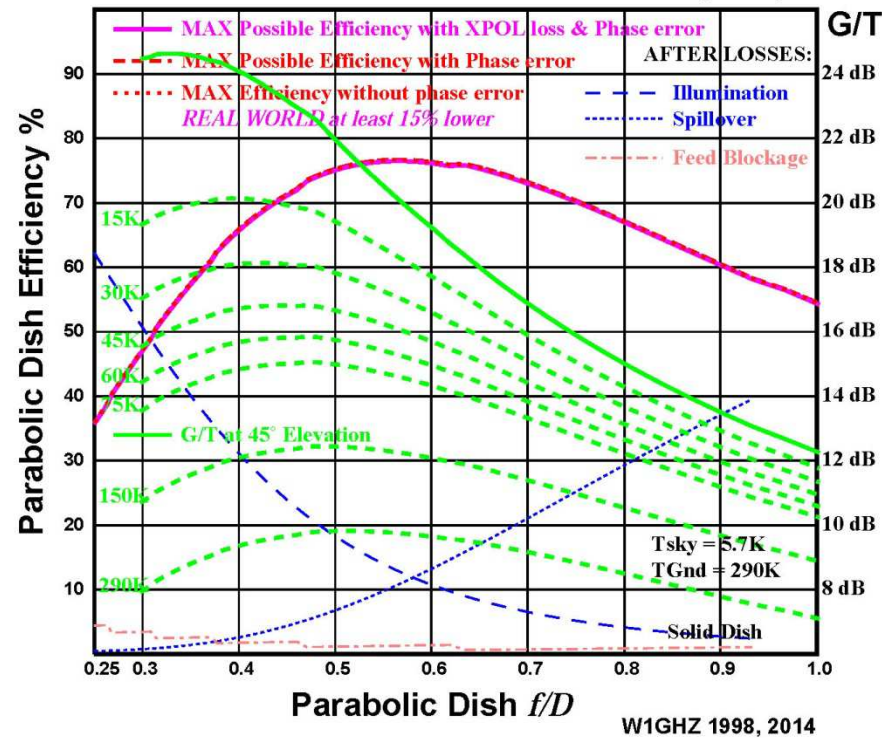
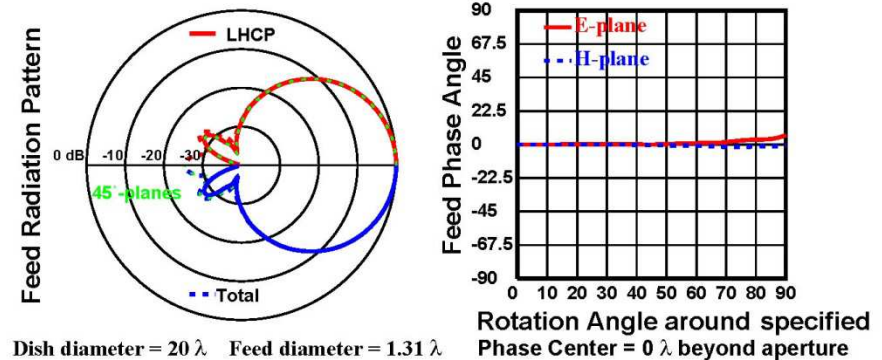
Figure 7



Effect of Receiver Noise Temperature

W2IMU Dual-mode Feed, 1.31λ diameter, LHCP
Receiver Noise Temp Comparison - 15,30,45,60,75,150 & 290K

Figure 8



Effect of Receiver Noise Temperature

- Very low noise temperatures make a huge difference
- 0.1 dB change in NF \rightarrow 1 dB change in G/T
- Serious LNA should be specified in K, not NF

Dish Size

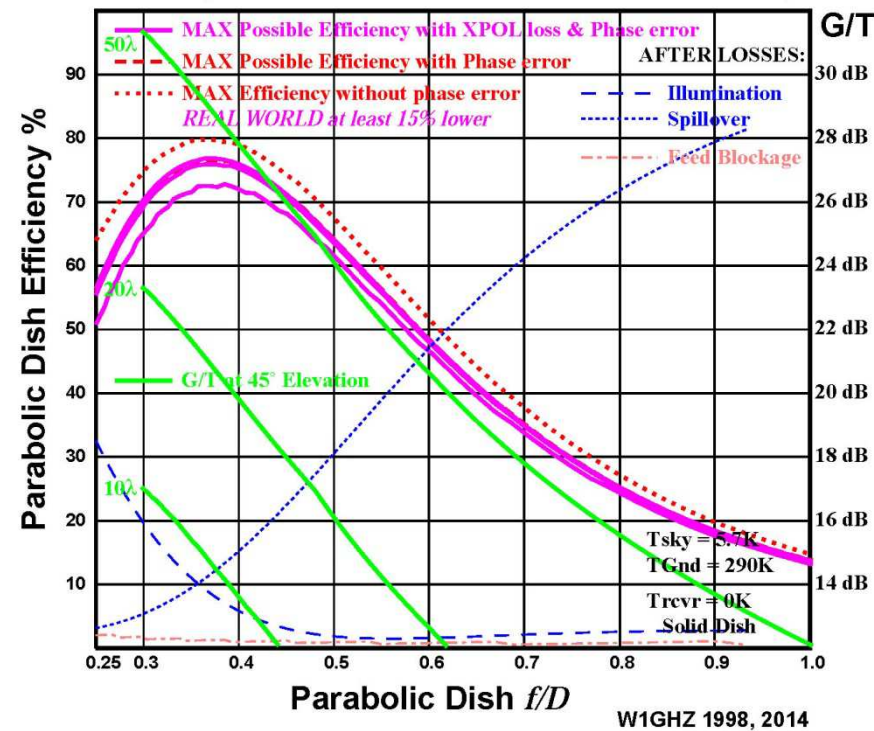
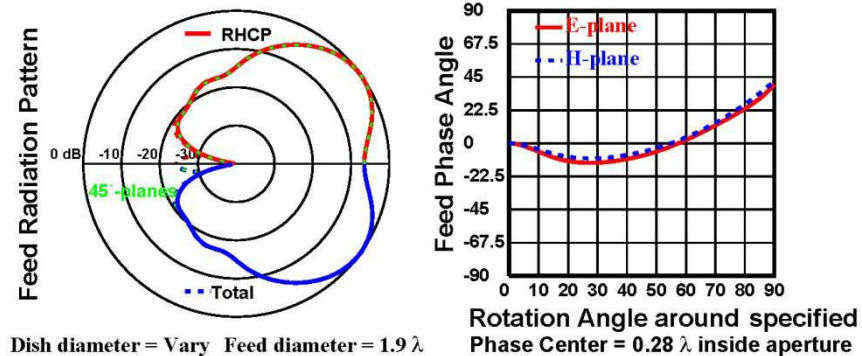
Gain proportional to size

Slight change in efficiency due to feed blockage

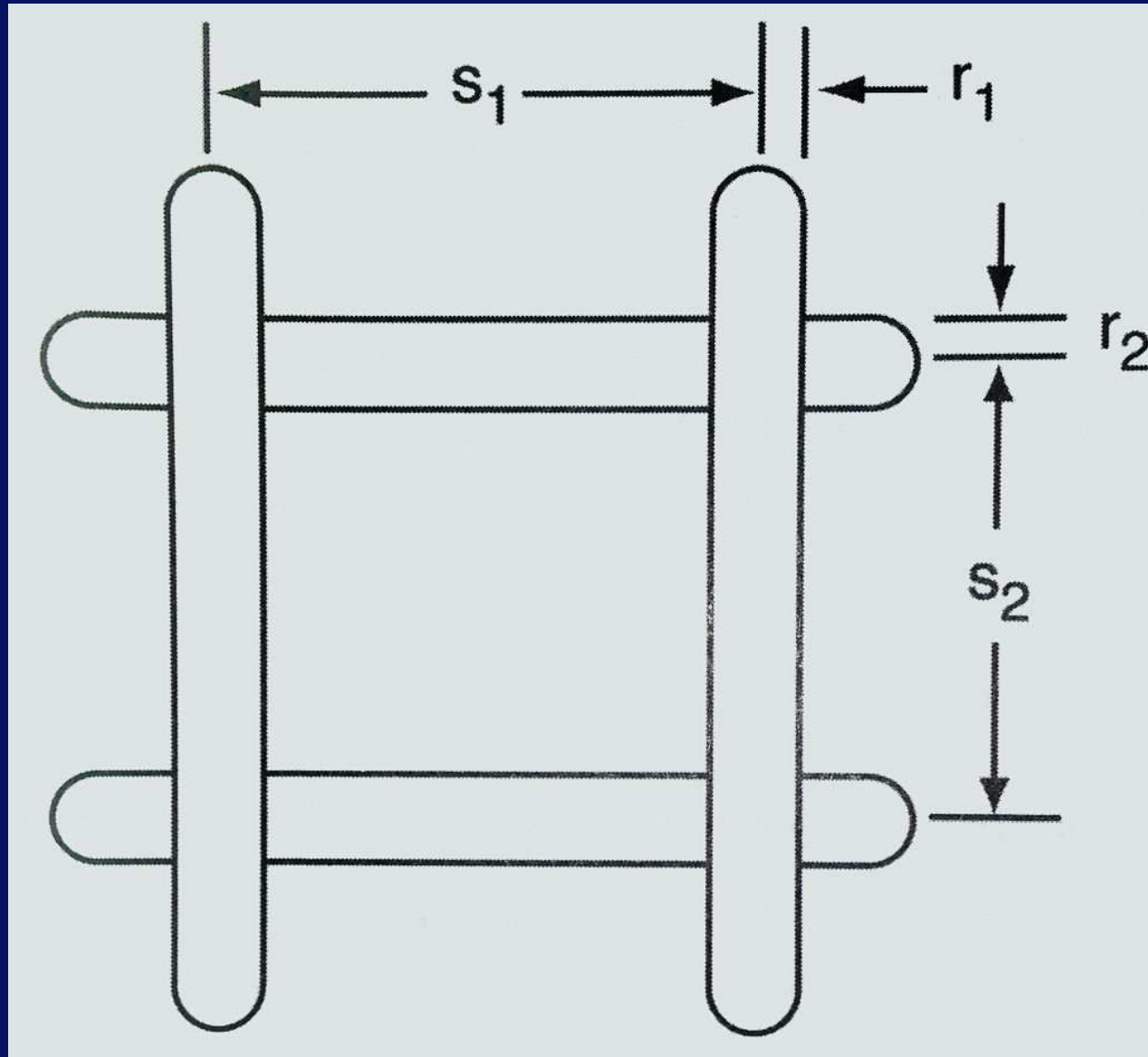
G/T follows gain

Super VE4MA, choke 0.6λ wide x 0.45λ deep, back 0.15λ
Dish Size Comparison - 10, 20, and 50λ Diameter

Figure 13



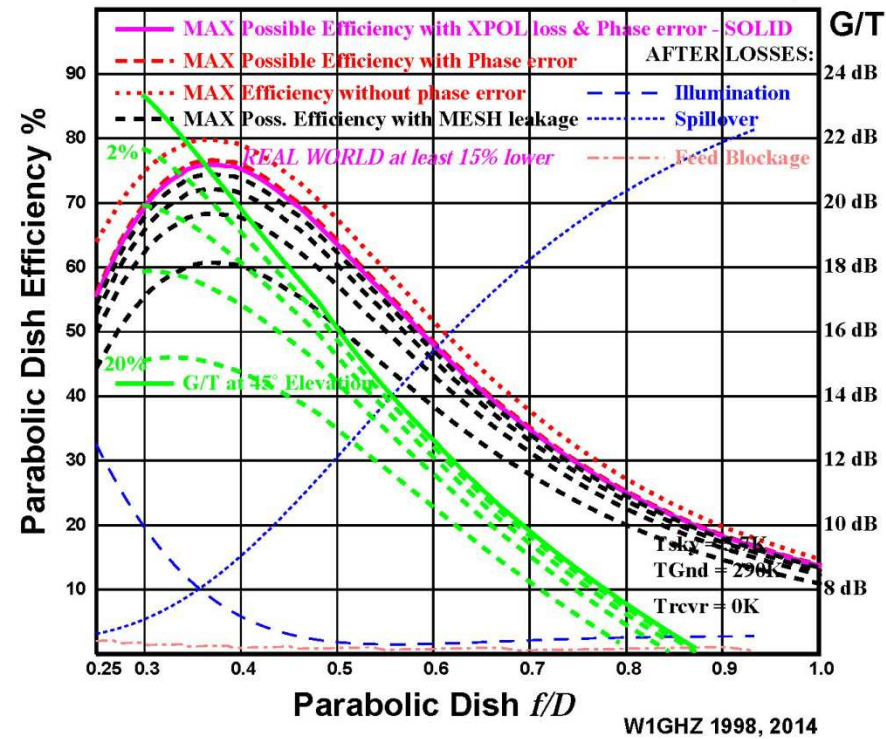
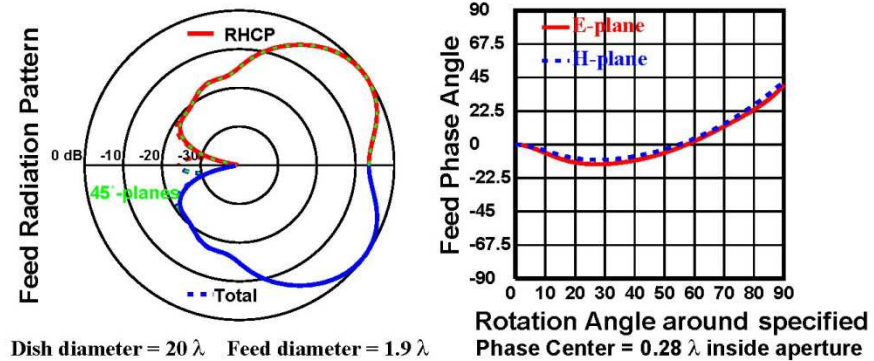
Mesh Reflector Leakage



Mesh Reflector

Super VE4MA, choke 0.6λ wide x 0.45λ deep, back 0.15λ
Mesh Dish Comparison - 2, 5, 10, and 20% Mesh Leakage

Figure 10

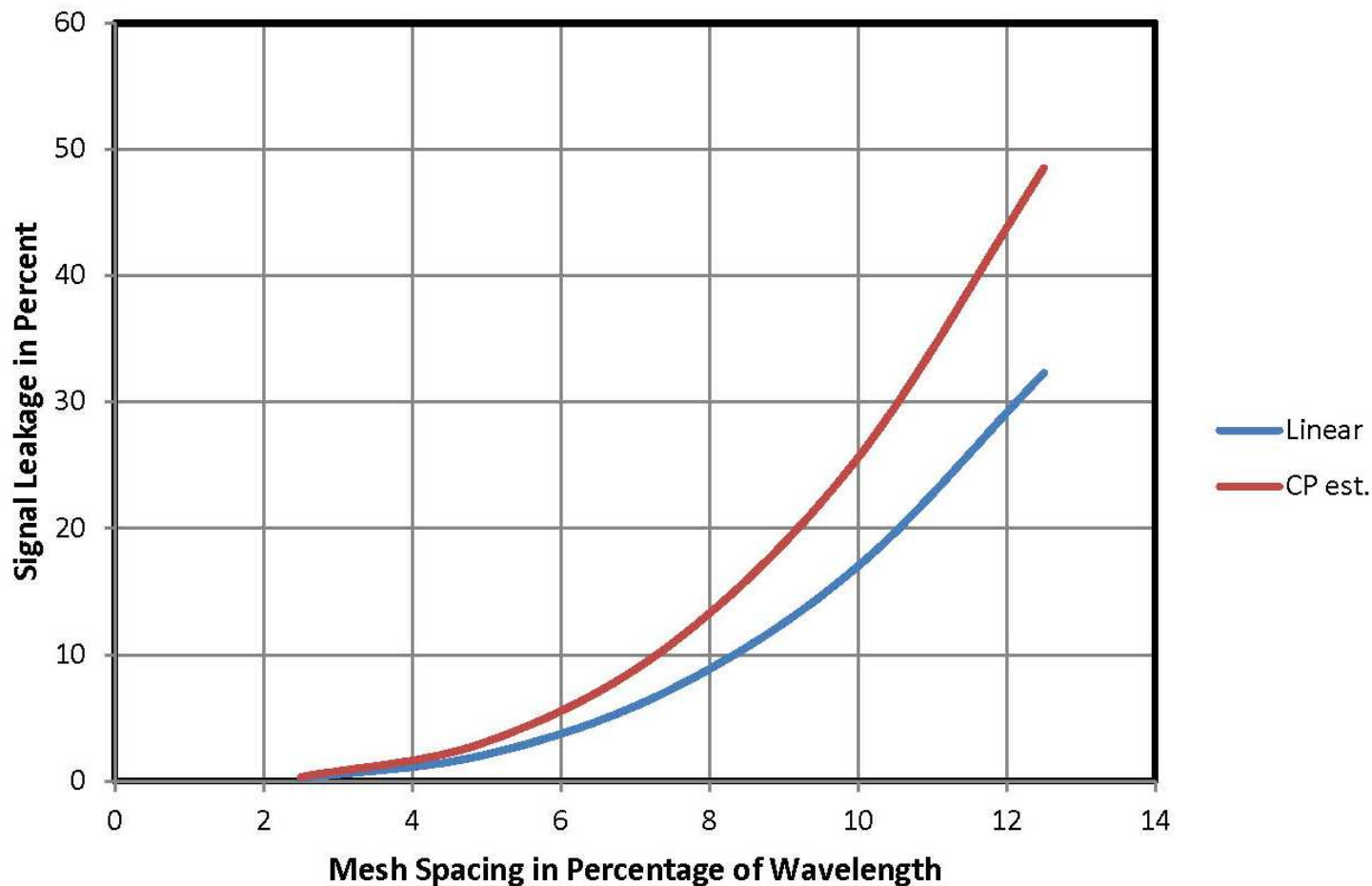


Mesh Reflector

- Mesh leakage reduces efficiency and gain
- Noise leaks through from ground at $\sim 290\text{K}$
- 20% leakage reduces gain by 1 dB, G/T by ~ 6 dB
- Adding mesh around edge without changing feedhorn
 - Reduces spillover noise – even with leakage
 - No effect on gain
 - Better G/T
 - Then increase TX power

Mesh Reflector Leakage Calculator on CD – from Otoshi

Leakage Through Mesh Surface



Feeds on CD

- VE4MA
- Super-VE4MA
- W2IMU dual-mode – several sizes
- RA3AQ – 042 (2008)
- Skobelev optimum dual mode – two sizes
- SM6FHZ CP Patch
- Coffee can (cylindrical waveguide)
- N2UO round septum - bare
- WA9HUV – cylindrical horn with flange
- OK1DFC square septum – bare and with flange

Program

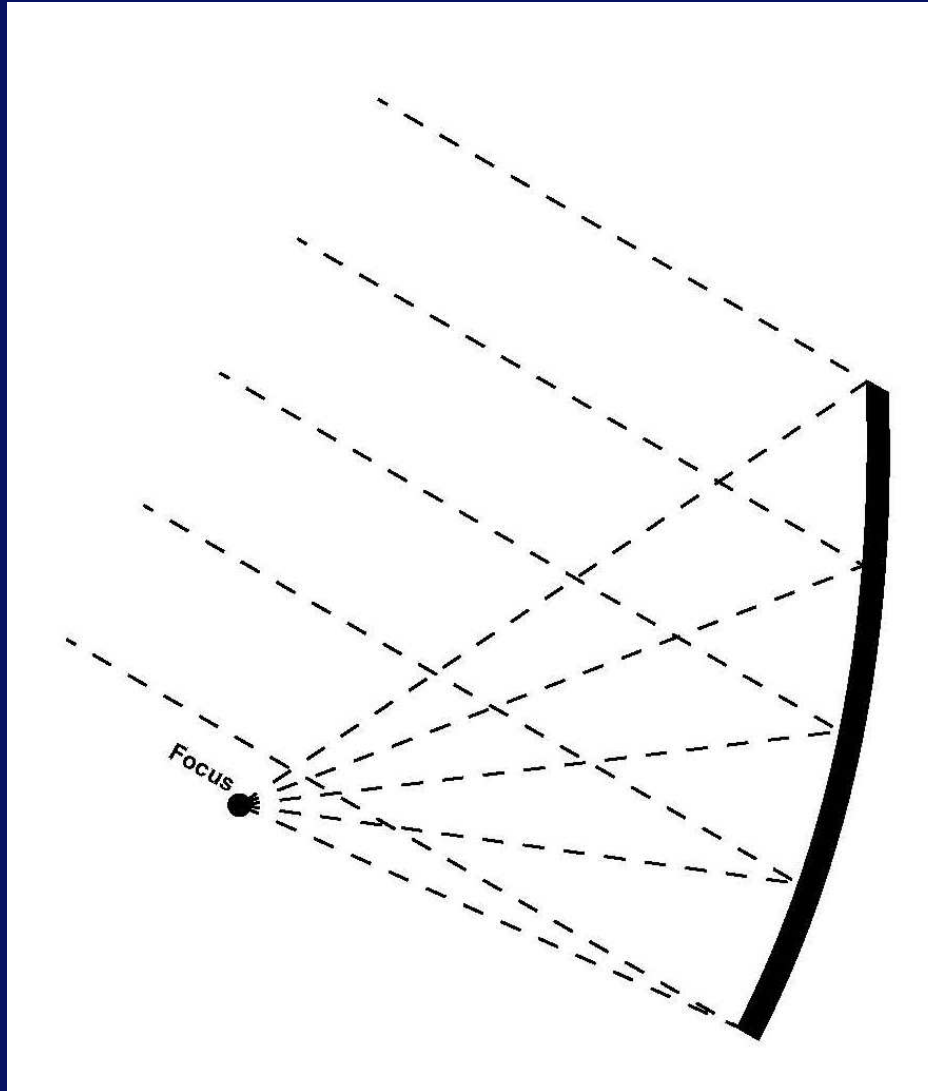
- Feed_GT.exe
 - Plots efficiency and G/T from feed patterns
 - Writes data to .csv file for spreadsheet
 - Feed pattern data available
 - Pattern data for new feeds
- Available at www.w1ghz.org

Offset Dishes

More complex
geometry

Elevation tilt more
complicated
- Spherical geometry

Have not written
code yet



G/T Summary

- Slight under-illumination for best G/T
- Optimize feed in dish
- Minimum T_{sys}
 - Preamp
 - Loss from feed to preamp
- Measure
- Serious EME dish should measure Celestial sources
 - Cassiopeia
 - Taurus
 - Cygnus

www.w1ghz.org

